ME 6402 – Lecture 18 Feedback linearization 3 (full-state feedback linearization)

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Overview:

- Introduce full-state feedback linearization
- Define a few basic concepts from differential geometry
- Frobenius Theorem

Additional Reading:

- Khalil, Chapter 13
- Sastry, Chapter 9

Review of Normal Form

To find the zero dynamics coordinates z, we must find n - r independent variables z such that \dot{z} does not contain u. An alternative approach is to find coordinates z_i (with i = 1, ..., n - r) such that:

$$\frac{\partial z_i}{\partial x}g(x) = \left[\frac{\partial z_i}{\partial x_1}\dots\frac{\partial z_i}{x_n}\right]g(x) \equiv 0$$

This can be interpreted as the coordinates z being chosen to be *normal* to the actuation vector g(x).

Example

Consider the system

$$\dot{x}_{1} = -x_{1} + \frac{2 + x_{3}^{2}}{1 + x_{3}^{2}}u$$
$$\dot{x}_{2} = x_{3}$$
$$\dot{x}_{3} = x_{1}x_{3} + u$$
$$y = x_{2}$$

We can inspect the relative degree of the system by observing:

$$y = x_2$$

$$\dot{y} = \dot{x}_2 = x_3$$

$$\ddot{y} = \dot{x}_3 = x_1 x_3 + u$$

Thus, the system has relative degree r = 2. Since r < n (and our system is SISO), we will have one degree of underactuation. To characterize the zero dynamics, we restrict x to:

$$Z = \{x \in \mathbb{R}^3 \text{ s.t. } x_2 = x_3 = 0\}$$

and take v = 0 for the input-output linearizing control law:

$$u^*(x) = \frac{1}{L_g L_f h(x)} \left(-L_f^2 h(x) + v \right)$$
$$= -x_1 x_3 + v$$
$$\implies u = -x_1 x_3$$

This yields the zero dynamics:

$$\dot{x}_1 = -x_1 + \frac{2 + x_3^2}{1 + x_3^2} \underbrace{(-x_1 x_3)}_{0} = -x_1$$
$$\dot{x}_2 = \underbrace{x_3}_{0} = 0$$
$$\dot{x}_3 = x_1 x_3 - x_1 x_3 = 0$$

Thus, the zero dynamics are $\dot{x}_1 = -x_1$.

Finally, to find the zero dynamics coordinate z for normal form, we need to find a function z(x) such that

$$z(0) = 0, \quad \frac{\partial z}{\partial x}g(x) = 0$$

Since $g(x) = [\frac{2+x_3^2}{1+x_3^2}, 0, 1]^T$:

$$\frac{\partial z_i}{\partial x}g(x) = 0 \implies \frac{\partial z}{\partial x_1} \cdot \frac{2 + x_3^2}{1 + x_3^2} + \frac{\partial z}{\partial x_3} = 0$$

This partial differential equation can be solved by separating variables to obtain

$$z(x) = -x_1 + x_3 + \tan^{-1}(x_3)$$

Thus, the normal form is:

$$T(x) = \begin{bmatrix} z \\ \zeta_1 \\ \zeta_2 \end{bmatrix} = \begin{bmatrix} z \\ \eta_1 \\ \eta_2 \end{bmatrix} = \begin{bmatrix} -x_1 + x_3 + \tan^{-1}(x_3) \\ x_2 \\ x_3 \end{bmatrix}$$

NOTE: From here on out I will be denoting the output coordinates as η instead of ζ since it is difficult for me to write ζ ...

Full-State Feedback Linearization

The system $\dot{x} = f(x) + g(x)u$, $x \in \mathbb{R}^n$, $u \in \mathbb{R}$, is (full state) feedback linearizable if a function $h : \mathbb{R}^n \to \mathbb{R}$ exists such that the relative degree from u to y = h(x) is n.

Since r = n, the normal form in Lecture 19 has no zero dynamics and

$$x \to \begin{bmatrix} \eta_1 \\ \eta_2 \\ \vdots \\ \eta_n \end{bmatrix} = \begin{bmatrix} h(x) \\ L_f h(x) \\ \vdots \\ L_f^{n-1} h(x) \end{bmatrix}$$

is a diffeomorphism that transforms the system to the form:

$$\dot{\eta}_1 = \eta_2$$

$$\dot{\eta}_2 = \eta_3$$

$$\vdots$$

$$\dot{\eta}_n = L_f^n h(x) + L_g L_f^{n-1} h(x) u.$$

Then, the feedback linearizing controller

$$u = \frac{1}{L_g L_f^{n-1} h(x)} \left(-L_f^n h(x) + v \right), \quad v = -k_1 \eta_1 \dots - k_n \eta_n,$$

yields the closed-loop system:

$$\dot{\eta} = A\eta \quad \text{where} \quad A = \begin{bmatrix} 0 & 1 & 0 & \dots & \\ 0 & 0 & 1 & \dots & \\ & & \ddots & \\ & & & \ddots & \\ & & & & 1 \\ -k_1 & -k_2 & -k_3 & \dots & -k_n \end{bmatrix}.$$

Example

Consider the system

$$\dot{x}_1 = x_2 + 2x_1^2$$

 $\dot{x}_2 = x_3 + u$
 $\dot{x}_3 = x_1 - x_3$

The choice $y = x_3$ gives relative degree r = n = 3. Thus, we know that the normal form will be of the form:

$$T(x) = \begin{bmatrix} \eta_1 \\ \eta_2 \\ \eta_3 \end{bmatrix} = \begin{bmatrix} h(x) \\ L_f h(x) \\ L_f^2 h(x) \end{bmatrix} = \begin{bmatrix} x_3 \\ x_1 - x_3 \\ x_2 + 2x_1^2 - (x_1 - x_3) \end{bmatrix}$$

This gives us our strict feedback form:

$$\dot{\eta} = \begin{bmatrix} \dot{\eta}_1 \\ \dot{\eta}_2 \\ \dot{\eta}_3 \end{bmatrix} = \begin{bmatrix} \eta_2 \\ \eta_3 \\ (4x_1 - 1)(x_2 + 2x_1^2) + x_1 + u \end{bmatrix}$$

with the feedback linearizing controller:

$$u = -(4x_1 - 1)(x_2 + 2x_1^2) - x_1 - k_1\eta_1 - k_2\eta_2 - k_3\eta_3.$$

Summary so far:

I/O Linearization:	 suitable for tracking
	• output <i>y</i> is an intrinsic physical variable
Full state linearization:	 set point stabilization
	• output is not intrinsic, selected to enable
	a linearizing change of variables.

Remaining question:

• When is a system feedback linearizable, *i.e.*, how do we know whether a relative degree *r* = *n* output exists?

Basic Definitions from Differential Geometry

<u>Definition</u>: The Lie bracket of two vector fields f and g is a new vector field defined as:

$$[f,g](x) = \frac{\partial g}{\partial x}f(x) - \frac{\partial f}{\partial x}g(x).$$

Note:

- 1. [f,g] = -[g,f],
- 2. [f, f] = 0,
- 3. If f, g are constant then [f, g] = 0.

Notation for repeated applications:

$$[f, [f, g]] = \operatorname{ad}_{f}^{2} g, \quad [f, [f, [f, g]]] = \operatorname{ad}_{f}^{3} g, \quad \cdots$$
$$\operatorname{ad}_{f}^{0} g(x) \triangleq g(x), \quad \operatorname{ad}_{f}^{k} g \triangleq [f, \operatorname{ad}_{f}^{k-1} g] \quad k = 1, 2, 3, \ldots$$

<u>Definition</u>: Given vector fields f_1, \ldots, f_k , a <u>distribution</u> Δ is defined as $\Delta(x) = \text{span}\{f_1(x), \ldots, f_k(x)\}.$

 $f \in \Delta$ means that there exist scalar functions $\alpha_i(x)$ such that

$$f(x) = \alpha_1(x)f_1(x) + \dots + \alpha_k(x)f_k(x).$$

<u>Definition</u>: Δ is said to be nonsingular if $f_1(x), \ldots, f_k(x)$ are linearly independent for all x.

Definition: Δ is said to be involutive if

$$g_1 \in \Delta, g_2 \in \Delta \implies [g_1, g_2] \in \Delta$$

that is, Δ is closed under the Lie bracket operation.

Proposition: $\Delta = \text{span}\{f_1, \dots, f_k\}$ is involutive if and only if

$$[f_i, f_j] \in \Delta \quad 1 \le i, j \le k.$$

Example 1: $\Delta = \text{span}\{f_1, \dots, f_k\}$ where f_1, \dots, f_k are constant vectors

Example 2: a single vector field f(x) is involutive since $[f, f] = 0 \in$ Δ

Definition: A nonsingular k-dimensional distribution

$$\Delta(x) = \operatorname{span}\{f_1(x), \dots, f_k(x)\} \quad x \in \mathbb{R}^n$$

is said to be completely integrable if there exist n - k functions

$$\phi_1(x),\ldots,\phi_{n-k}(x)$$

such that

$$\frac{\partial \phi_i}{\partial x} f_j(x) = 0 \quad i = 1, \dots, n-k, \quad j = 1, \dots, k$$

and $d\Phi_i(x) := \frac{\partial \phi_i}{\partial x}$, $i = 1, \dots, n-k$, are linearly independent.

Frobenius Theorem: A nonsingular distribution is completely integrable if and only if it is involutive.

Back to (Full State) Feedback Linearization

<u>Recall</u>: $\dot{x} = f(x) + g(x)u, x \in \mathbb{R}^n, u \in \mathbb{R}$ is feedback linearizable if we can find an output y = h(x) such that relative degree r = n.

How do we determine if a relative degree r = n output exists?

$$L_g h(x) = L_g L_f h(x) = \dots = L_g L_f^{n-2} h(x) = 0 \text{ in a nbhd of } x_0 \quad (1)$$
$$L_g L_f^{n-1} h(x_0) \neq 0. \quad (2)$$

$$L_g L_f^{n-1} h(x_0) \neq 0.$$
 (2)

Proposition:¹ (1)-(2) are equivalent to:

$$L_g h(x) = L_{\mathrm{ad}_f g} h(x) = \dots = L_{\mathrm{ad}_f^{n-2} g} h(x) = 0 \text{ in a nbhd of } x_0 \quad (3)$$

$$L_{\mathrm{ad}_f^{n-1}g}h(x_0) \neq 0. \tag{4}$$

¹ follows from (5) below with j = 0

The advantage of (3) over (1) is that it has the form:

$$\frac{\partial h}{\partial x}[g(x) \quad \mathrm{ad}_f g(x) \quad \dots \quad \mathrm{ad}_f^{n-2}g(x)] = 0$$

which is amenable to the Frobenius Theorem.

<u>Theorem</u>: $\dot{x} = f(x) + g(x)u$ is feedback linearizable around x_0 if and only if the following two conditions hold:

C1) $[g(x_0) \text{ ad}_f g(x_0) \dots \text{ ad}_f^{n-1} g(x_0)]$ has rank n

C2) $\Delta(x) = \operatorname{span}\{g(x), \operatorname{ad}_f g(x), \dots, \operatorname{ad}_f^{n-2} g(x)\}$ is involutive in a neighborhood of x_0 .

<u>Proof:</u> (if) Given C1 and C2 show that there exists h(x) satisfying (3)-(4).

 $\Delta(x)$ is nonsingular by C1 and involutive by C2. Thus, by the Frobenius Theorem, there exists h(x) satisfying (3) and $dh(x) \neq 0$.

To prove (4) suppose, to the contrary, $L_{\mathrm{ad}_{f}^{n-1}}h(x_{0})=0$. This implies

$$dh(x_0)[g(x_0) \quad \text{ad}_f g(x_0) \quad \dots \quad \text{ad}_f^{n-1}g(x_0)] = 0.$$
nonsingular by C1

Thus $dh(x_0) = 0$, a contradiction.

(only if) Given that y = h(x) with r = n exists, that is (3)-(4) hold, show that C1 and C2 are true.

We will use the following fact² which holds when r = n:

$$L_{\mathrm{ad}_{f}^{i}g}L_{f}^{j}h(x) = \begin{cases} 0 & \text{if } i+j \leq n-2\\ (-1)^{n-1-j}L_{g}L_{f}^{n-1}h(x) \neq 0 & \text{if } i+j = n-1. \end{cases}$$
(5)

Define the matrix

$$M = \begin{bmatrix} dh \\ dL_fh \\ \vdots \\ dL_f^{n-1}h \end{bmatrix} \begin{bmatrix} g & -\operatorname{ad}_f g & \operatorname{ad}_f^2 g & \dots & (-1)^{n-1}\operatorname{ad}_f^{n-1}g \end{bmatrix}$$
(6)

and note that the (k, ℓ) entry is:

$$\begin{split} M_{k\ell} &= dL_f^{k-1} h(x) (-1)^{\ell-1} \operatorname{ad}_f^{\ell-1} g(x) \\ &= (-1)^{\ell-1} L_{\operatorname{ad}_f^{\ell-1} g} L_f^{k-1} h(x). \end{split}$$

Then, from (5):

In practice, we use the Frobenius Theorem to show that the distribution $\Delta(x)$ is involutive by finding a function $\phi(x)$ such that $\frac{\partial \phi}{\partial x}[g(x), \operatorname{ad}_f g(x), \dots, \operatorname{ad}_f^{n-2}g(x)] \equiv 0.$

² see, e.g., Khalil, Lemma C.8

 $\begin{bmatrix} 0 & 0 & \cdots & \star \end{bmatrix}$

Since the diagonal entries are nonzero, M has rank n and thus the factor

$$g - \operatorname{ad}_f g \operatorname{ad}_f^2 g \ldots (-1)^{n-1} \operatorname{ad}_f^{n-1} g$$

in (6) must have rank n as well. Thus C1 follows.

This also implies $\Delta(x)$ is nonsingular; thus, by the Frobenius Thm,

complete integrability \equiv involutivity.

 $\Delta(x)$ is completely integrable since h(x) satisfying (3) exists by assumption; thus, we conclude involutivity (C2).

Example:

 $\dot{x}_1 = x_2 + 2x_1^2$ $\dot{x}_2 = x_3 + u$ $\dot{x}_3 = x_1 - x_3$

Feedback linearizability was shown on page 1 by inspection: $y = x_3$ gives relative degree = 3. Verify with the theorem above:

$$f(x) = \begin{bmatrix} x_2 + 2x_1^2 \\ x_3 \\ x_1 - x_3 \end{bmatrix} \quad g(x) = \begin{bmatrix} 0 \\ 1 \\ 0 \end{bmatrix}$$
$$[f,g](x) = \begin{bmatrix} -1 \\ 0 \\ 0 \end{bmatrix} \quad [f,[f,g]](x) = \begin{bmatrix} 4x_1 \\ 0 \\ 1 \end{bmatrix}$$

Recall that $[f,g] = \frac{\partial g}{\partial x}f(x) - \frac{\partial f}{\partial x}g(x)$ $[f,g] = 0 - \begin{bmatrix} 4x_1 & 1 & 0\\ 0 & 0 & 1\\ 1 & 0 & -1 \end{bmatrix} \begin{bmatrix} 0\\ 1\\ 0 \end{bmatrix} = \begin{bmatrix} -1\\ 0\\ 0 \end{bmatrix}$ $[f,[f,g]] = 0 - \begin{bmatrix} 4x_1 & 1 & 0\\ 0 & 0 & 1\\ 1 & 0 & -1 \end{bmatrix} \begin{bmatrix} -1\\ 0\\ 0 \end{bmatrix} = \begin{bmatrix} 4x_1\\ 0\\ 1 \end{bmatrix}$

Conditions of the theorem:

1.
$$\begin{bmatrix} 0 & -1 & 4x_1 \\ 1 & 0 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$
 full rank
2.
$$\Delta = \operatorname{span} \left\{ \begin{bmatrix} 0 \\ 1 \\ 0 \end{bmatrix}, \begin{bmatrix} -1 \\ 0 \\ 0 \end{bmatrix} \right\}$$
 involutive

$$\frac{\partial h}{\partial x} \begin{bmatrix} 0 & -1 \\ 1 & 0 \\ 0 & 0 \end{bmatrix}$$
 satisfied by $h(x) = x_3$.